

**PHOTOMULTIPLIER TUBE  
BASE-PREAMPLIFIER  
Model 2007P**

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0985

**Operator's Manual**

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# Section 1. Introduction

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## 1.1 INTRODUCTION

The Canberra Model 2007P Tube Base-Preamplifier provides the high voltage divider network for correctly biasing essentially all 10-stage photomultiplier tubes (PMT) used for nuclear spectroscopy. This network is intended for use with a positive high voltage for tubes which operate with their photocathodes near ground potential. The network includes a focus control for adjusting the detector resolution performance, and a gain trim control for matching outputs of several detectors when used in arrays.

Designed to be compatible with the Canberra Model 802 series Scintillation Detectors (or equivalent), the tube base connects directly to the pins of the PMT, providing a compact integrally mounted assembly.

The Canberra Model 2007P Tube Base-Preamplifier also contains a low noise charge-sensitive preamplifier. The

preamplifier recovers the charge pulse at the anode pin of the PMT directly and converts it to a positive voltage pulse output. The peak amplitude of each output pulse is linearly proportional to the total charge output of the PMT during each amplified photo event. The pulse is set to decay at a nominal 50  $\mu$ sec time constant, and interfaces directly with any of Canberra's spectroscopy amplifiers.

The Model 2007P includes a diode protection network on the preamplifier input to prevent damage to the circuitry from the inadvertent sudden application or removal of PMT bias voltage. A test input is also provided to aid system testing, gain calibration, or troubleshooting. Preamplifier power is usually derived from the associated pulse shaping amplifier. A ten-foot long power cable is supplied with the Model 2007P.

# Section 2. Specifications

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## 2.1 INPUTS

**DETECTOR**—The preamplifier is internally connected to pin 11 of the Tube Base socket (PMT anode).

**TEST INPUT**—Accepts a positive - or negative - polarity tail pulse from a test-pulse generator. Charge coupled at 30 picocoulombs per volt to preamplifier input. Voltage gain to output is 130 mV/V nominal. Input impedance is  $\approx$  93 ohms.

**HV INPUT**—PMT bias-voltage range, 0 to + 2000 V dc. Anode series resistance 1M ohms. Bias network total resistance: 6.66 M ohms to 7.16 M ohms, depending on the position of the GAIN control.

## 2.2 OUTPUTS

**ENERGY OUTPUT**—Provides unipolar positive pulses linearly proportional in peak amplitude to charge delivered at PMT anode.

Decay time constant 50 microseconds nominal. Rise time less than 20 nanoseconds. Delivers up to 10 V peak. Output impedance  $\approx$  93 ohms, series connected; direct coupled.

## 2.3 PERFORMANCE

**INTEGRAL NON-LINEARITY**—less than  $\pm$  0.04% for up to 10 volt output.

**GAIN DRIFT**—Less than  $\pm$  0.01%/°C ( $\pm$  100 ppm/°C).

**NOISE**—Less than  $1 \times 10^{-16}$  coulombs rms referred to input.

**CHARGE SENSITIVITY**—4.5 mV/picocoulomb

## 2.4 CONNECTOR TYPES

**HIGH VOLTAGE**—SHV

**ENERGY OUTPUT, TEST INPUT**—BNC

**TUBE SOCKET**—14-pin (Cinch Jones 3M-14 or equivalent)

**POWER**—Amphenol 17-20090

## 2.5 CONTROLS

**FOCUS**—Single-turn screwdriver adjusted potentiometer to adjust voltage at grid of PMT. Range 72 to 145 V per 1000 V dc of high voltage input.

**GAIN**—Single-turn screwdriver adjusted rheostat to adjust anode bias. Adjustment range: 92% to 100% of applied high voltage.

## 2.6 POWER REQUIREMENTS

**HIGH VOLTAGE**—Bias network requires 150  $\mu$ A per 1000 V dc

$\pm$  12 V dc—15 mA dc nominal

## 2.7 PHYSICAL

**SIZE**—Diameter 5.8 cm (2.3 in.)

**LENGTH**—7.6 cm (3.0 in.)

**NET WEIGHT**—0.7 kg (1.5 lb.)

## Section 3. Installation

### 3.1 GENERAL

The Model 2007P is intended to provide a convenient package for interfacing with the photomultiplier tube (PMT). As specific mounting details differ significantly between applications, only the following general considerations can be offered.

### 3.2 DETECTOR MOUNTING

The tube base preamp is intended to mount coaxially with the Model 802 series scintillation detectors simply by mating the PMT pins into the tube socket. The scintillator should, of course, be handled with care in mating, and protected from shock.

### 3.3 PRECAUTIONS

Consistent with good operating practice for the PMT, the high voltage full bias should not be applied immediately; it should be raised and lowered over several seconds. The Model 2007P is diode protected for occasional faults and for high-voltage arcing. A primary consideration here will be the instantaneous noise current in the PMT, which may take a considerable time to settle.

Steady state dissipation in the PMT bias network has been minimized, in order to prevent degradation of background "dark" currents due to local heating. Hence no particular care need be expended in providing any heat sinking for the tube base.

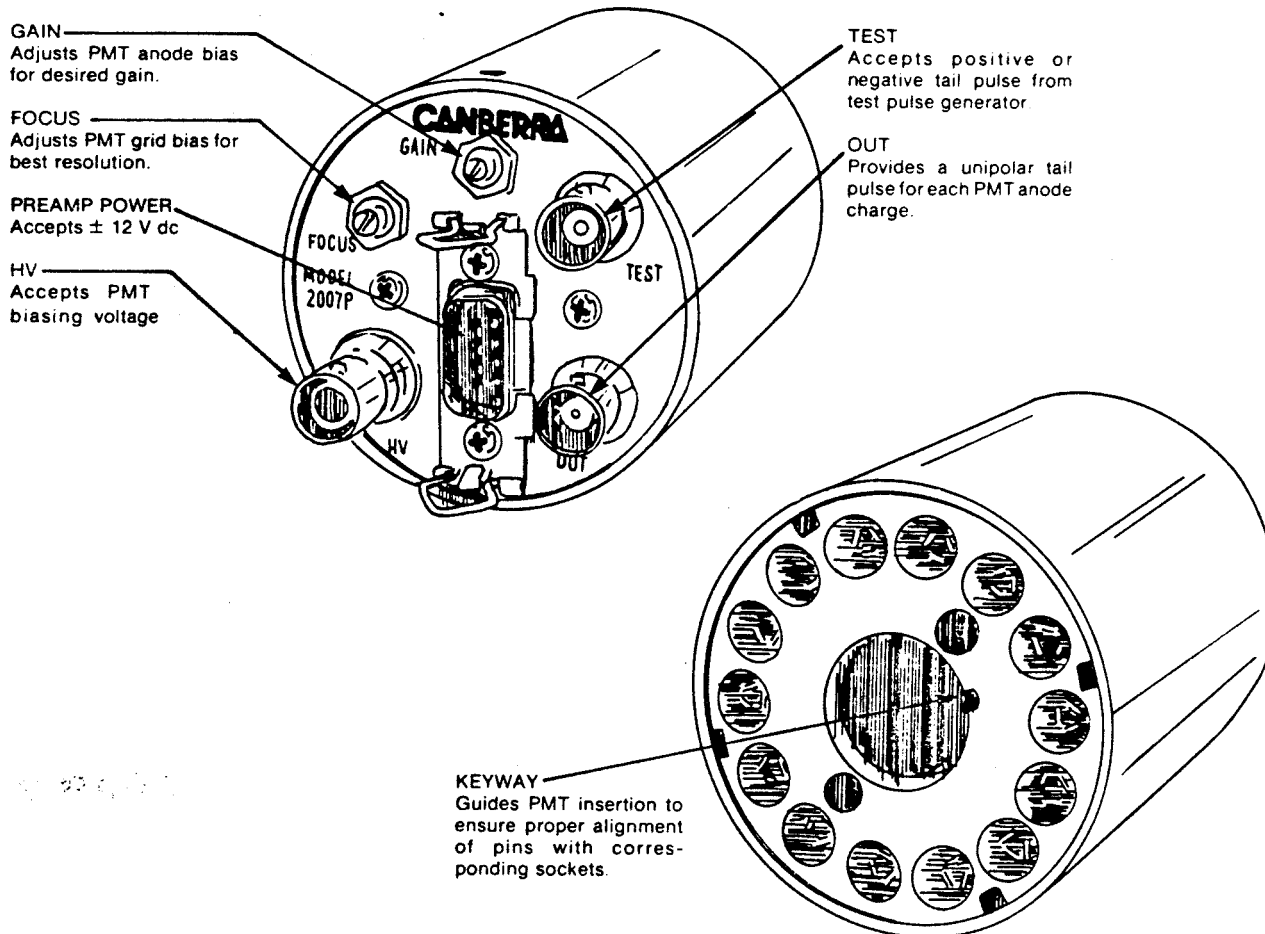


Figure 2-1  
Model 2007P  
Front and Rear Panels

## Section 4. Operating Instructions

### 4.1 GENERAL

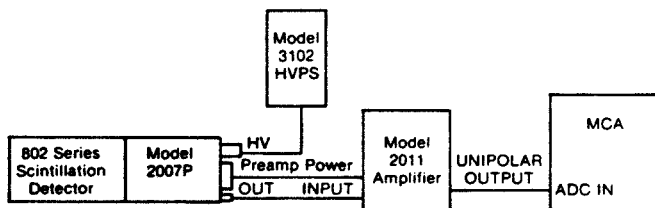
The purpose of this section is to familiarize the user with a typical setup incorporating the Model 2007P Photomultiplier Tube Base/Preamplifier. The following discussion of a typical configuration will give the user sufficient familiarity with the Model 2007P to permit its proper use in any system.

### 4.2 SETUP

Connect the Model 2007P to the Photomultiplier Tube (PMT). Be certain to align the key on the PMT with the keyway on the Model 2007P before attempting to insert the PMT pins into the tube base socket. See the rear panel photograph (Figure 2-1) for the location of the keyway.

Using a small screwdriver, turn the Model 2007P GAIN control to its extreme clockwise position, which will provide the highest possible gain, and adjust the FOCUS control to about mid-range.

Connect a high-voltage cable between the Model 2007P HV connector and the High Voltage Power Supply. Connect a signal cable between the Model 2007P OUT connector and the amplifier's input. Connect the preamplifier power cable between the preamp power (9-pin) connectors on the Model 2007P and the amplifier. Note that for a PMT, the amplifier must be capable of 0.5  $\mu$  sec shaping.



**Model 2007P in a Typical System**  
Figure 4-1

### 4.3 THE GAIN CONTROL

The GAIN control is used to match the gain of two or more PMTs in a multiple detector system. If a single PMT is being used, the control should be left in the extreme clockwise position.

To match the gain of several PMTs, it is necessary to know the gain of each detector. Collect several thousand counts in a peak of  $^{137}\text{Cs}$  (for instance) and record the number of the peak channel. Repeat for each PMT.

Place the MCA's cursor in the lowest recorded channel found in the preceding paragraph and adjust the GAIN controls of each PMT in turn so that all will collect the peak in that same peak channel.

### 4.4 THE FOCUS CONTROL

The FOCUS control is used to obtain the best possible resolution with a given PMT. Resolution is defined as the ability of the detector to differentiate between two peaks that are close together in energy. Thus the narrower the peak the better the peak separation and the better the resolution.

Start with the FOCUS control set about the middle of its range. By checking the resolution several times with a slight adjustment of the FOCUS control each time, the point of best resolution can be found.

### 4.5 RESOLUTION

The full width of the peak at half of its maximum value (FWHM) is used to determine the resolution by:

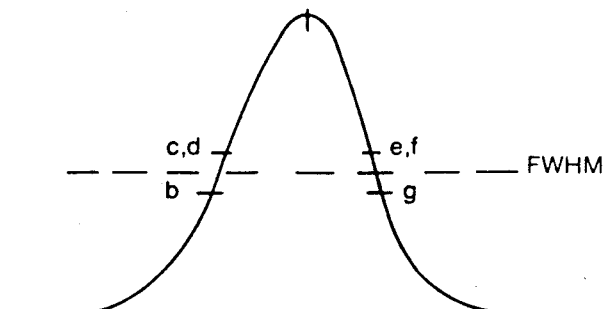
$$\text{Resolution} = \frac{\text{FWHM}}{\text{Peak Position}}$$

where Peak Position and FWHM are expressed in channels. The performance of a scintillation detector is usually specified in terms of its resolution for the 662 keV peak of  $^{137}\text{Cesium}$ .

To determine the resolution, collect a peak of 10 000 counts of  $^{137}\text{Cs}$ . Half maximum of the peak would be 5 000 counts, but it is unlikely that there will be a channel that contains exactly 5 000 counts. Therefore, it is necessary to interpolate the data.

Record the following information:

- The peak channel. That is, the channel with 10 000 counts.
- The counts in the channel just below FWHM on the left side of the peak. Counts < 5 000.
- The counts in the channel at or just above FWHM on the left side of the peak. Counts  $\geq$  5 000.
- The number of the channel at or just above FWHM on the left side of the peak.
- The number of the channel at or just above FWHM on the right side of the peak.
- The counts in the channel at or just above FWHM on the right side of the peak. Counts  $\geq$  5 000.
- The counts in the channel just below FWHM on the right side of the peak. Counts < 5 000.



**Figure 4-2**

Using the information gathered above, apply the following formula:

$$\frac{e-d + \frac{b}{c} + \frac{f}{g}}{a} = \text{resolution expressed as a decimal fraction.}$$

The resolution will be in the range of 0.06 to 0.09 (6% to 9%) for a Canberra Series 802 Scintillation Detector.

By adjusting the FOCUS control slightly to one side or the other of mid-range and doing another resolution check, it will be apparent that the resolution has been improved (the number is smaller) or has been degraded (the number is larger).

By doing several successive approximations, the best resolution will be found. The FOCUS control can be left in that position as long as the same PMT and Model 2007P are associated. It would be helpful however, to check for best resolution from time to time to be sure that there is no change with time.

## Section 5. Theory of Operation

### 5.1 GENERAL

The Model 2007P essentially consists of two functionally separate sections. The voltage divider provides the photomultiplier tube (PMT) with the proper operating potentials and the preamplifier converts the charge output of the PMT into a proportional voltage.

Specifically, the bias network chosen for the PMT provides the nominal distribution of accelerating potentials between dynode sections that has found to yield the best performance for nuclear applications. Capacitors C9 and C10, provided between the anode and upper two dynodes, bypass large signal current occurring under moderately high pulse amplitude conditions. RV3 permits independent control of PMT grid potential for optimization of resolution, while RV2 permits PMT gain to be adjusted by modifying the potential applied at the top of the divider string.

The preamplifier section functions as an operational integrator with Q1 in the common source configuration providing a high open loop gain by virtue of the ac bootstrap action furnished by C5. Q1 also allows a high input impedance by virtue of its gate input, while Q2 provides current gain and low output impedance. The loop is then closed by the integrating capacitor C3, with R5 providing dc stability in addition to facilitating the discharge of C3. RV1 enables the adjustment of output dc offset at the same time allowing the gate of Q1 to be biased slightly negative.

The sensitivity of the preamp to charge may be calculated by noting that all charge transferred from the PMT anode through C2 collects on C3, creating a potential difference across C3 according to the relation,

$$Q = CV \text{ or } V/Q = 1/C3$$

For the 2007P since  $C3 = 220 \text{ pF}$ ,

$$V/Q = 1/220 \text{ pF} = 4.5 \text{ mV/pC}$$

Filtering of the HV input is provided by C8 while standard LC decoupling of the low voltage supply lines is employed to minimize problems caused by noise pickup in the power cable.

### 5.2 EQUIPMENT REQUIRED FOR CHECKOUT

1. Calibrated dual trace Oscilloscope (scope), rated dc-100 MHz minimum, with vertical sensitivity of at least 50 mV/cm and a time base sweep of at least 20 ns/cm.
2. Reference Pulser with a rise time less than 20 nsec (Canberra Model 1407 or equivalent).
3. High Voltage Power Supply (HVPS).
4. DC Voltmeter (DVM) with rated accuracy to 0.1% with a 10M ohm input impedance.
5. Model 2000 NIM Bin and Power Supply, or equivalent.
6. Preamplifier power source with Preamp Power Connector. Note that all Canberra amplifiers are equipped with preamp power connectors.
7. Shielded coaxial cable, RG-62, BNC-BNC as required, lengths as short as practicable, herein referred to as "coax".
8. Shielded coaxial cable, RG-59, SHV-SHV as required, lengths as short as practicable, herein referred to as "HV coax".

### 5.3 INITIAL SETUP FOR CHECKOUT

1. Model 2007P:
 

GAIN	fully CW
FOCUS	fully CCW
2. Model 1407 Pulser:
 

RISE TIME	MIN
FALL TIME	400 $\mu$ sec
ATTENUATION	X2
LINE/OFF/90Hz	90 Hz
NORMALIZE	fully CW
POS/NEG	NEG
3. Oscilloscope
 

CHANNEL 1	1 V/cm
CHANNEL 2	50 mV/cm
DISPLAY	ALT, EXT TRIG
SLOPE	(-)
TIME BASE	20 $\mu$ sec/cm

#### 4 CHECKOUT PROCEDURE

1. Connect the preamp power cable from the 2007P to the source of preamp power.
2. Using a length of coax, connect the OUTPUT of the 2007P to channel 2 of the scope.
3. Apply power to the 2007P and verify the dc level on the scope channel 2 trace is  $0 \pm 50$  mV.
4. Connect the 1407 NORMAL output to the scope external trigger input and the 1407 ATTEN output to the scope channel 1 input using suitable coax lengths.
5. Adjust the 1407 PULSE HEIGHT control for a -5V signal on the channel 1 trace.
6. Remove the cable from the Scope channel 1 input and connect it to the 2007P TEST input.
7. Move the cable from the scope channel 2 input to channel 1 input and set the channel 1 range to 0.2 V/cm.
8. Verify the signal on the channel 1 trace to be  $> +1$  volt.
9. Adjust the 1407 PULSE HEIGHT control for a 1 V signal on the channel 1 trace.
10. Verify the slow fall time from 1 V peak to 360 mV to be between 35 and 65  $\mu$ sec.
11. Expand the scope time base to 10 nsec/cm and verify the fast rise time from the 10 - 90% levels to be  $< 20$  nsec.

12. Disconnect all coax from the 2007P and using HV coax connect the HVPS to the HV connector on the 2007P.
13. Make sure the 2007P is resting on a nonconductive surface and increase HVPS to +100 V dc.
14. Use the DVM to measure the potential, with respect to chassis ground (pin 14), of each pin in the 2007P socket. The range of acceptable potentials is given below in dc volts.

PIN	1	13	-	15.4	8	63.1 - 69.7
	2	20.7	-	22.9	9	72.2 - 79.9
	3	27.4	-	30.2	10	80.8 - 91.6
	4	33.7	-	37.3	11	89.8 - 99.2
	5	40.5	-	44.7	12	no connection
	6	47.4	-	52.4	13	7.6 - 8.4
	7	54.8	-	60.6	14	ground

15. Turn the FOCUS control to CW. Pin 13 should now be 14 to 15.4 V. Turn GAIN control to CCW. Pin 10 should now be 70.9 to 82.7 V. Reduce HVPS to zero and turn OFF.

This warranty covers Canberra equipment shipped to customers within the United States. For equipment shipped outside the United States, a similar warranty is provided by Canberra's local representative.

### **DOMESTIC WARRANTY**

Equipment manufactured by Canberra's Instruments Division, Detector Products Division, and Nuclear Data Systems Division is warranted against defects in materials and workmanship for one year from the date of shipment. This warranty does not cover damage caused by improper use of the equipment.

If defects are discovered within 30 days of the time you receive the equipment, Canberra will pay transportation costs both ways. After the first 30 days, you will have to pay the transportation costs.

Canberra's software media are warranted to be free from defects for 90 days from the date of shipment.

This is the only warranty provided by Canberra; there are no other warranties, expressed or implied. All warranties of merchantability and fitness for an intended purpose are excluded. Canberra shall have no liability for any special, indirect or consequential damages caused by failure of any equipment manufactured by Canberra.

### **EXCLUSIONS**

This warranty does not cover equipment which has been modified without Canberra's written permission or which has been subjected to unusual physical or electrical stress as determined by Canberra's Service Personnel.

Canberra is under no obligation to provide warranty service if adjustment, repair, or parts replacement is required because of damage caused by other than ordinary use or if the equipment is serviced or repaired or if attempts are made to service or repair equipment by other than Canberra personnel without the prior approval of Canberra.

This warranty does not cover detector damage caused by abuse, neutrons, or heavy charged particles. Damage from these causes is readily identifiable, as described in the manual accompanying each detector.

Equipment provided by Canberra from other manufacturers will carry the warranties provided by those manufacturers unless this equipment is specifically covered under a separate service contract.

### **SHIPPING DAMAGE**

Examine shipments carefully when you receive them for evidence of damage caused in transit. If damage is found, notify Canberra and the carrier immediately. Keep all packages, materials and documents, including your freight bill, invoice and packing list. Although Canberra is not responsible for damage sustained in transit, we will be glad to help you in processing your claim.

### **OUT OF WARRANTY REPAIRS**

Any Canberra equipment which is no longer covered by warranty may be returned to Canberra freight prepaid for repair. After the

equipment is repaired, it will pass through our normal pre-shipment checkout procedure.

### **RETURNING EQUIPMENT**

Before returning equipment other than detectors for repair you must contact your Regional Service Center or one of our factories for instructions.

For detector repair, contact the Canberra Detector Division in our Meriden, Connecticut factory for instructions.

If you are going to return the equipment to the factory, you must call first to get an Authorized Return Number (ARN).

Any shipment received without an ARN will not be processed or repaired until you contact us with the necessary information.

When you call us, we will be glad to suggest the best way for you to ship the equipment and will expedite the shipment in case it is lost or delayed in transit. Giving you shipping advice does not make us responsible in any way for the equipment while it is in transit.

Please pack your equipment carefully so it won't be damaged in shipment. The original shipping material is best for this purpose, but if you don't have it, Canberra will be glad to provide a suitable container for a fee.

### **SERVICE OPTIONS**

Canberra has a comprehensive Service Program which provides several options for your equipment maintenance needs:

- On-site Maintenance Agreements for system users who require the highest level of service.
- Extended Warranty Agreements for customers who need a rapid response, low cost, fixed fee repair service.
- Essential Software Service Agreements designed to assist users who want continuous technical assistance or software updates as they occur.
- Standard return-to-factory service options.
- A full line of quality replacement parts for customers who elect to maintain their own equipment.
- A Field Communications Center to provide over-the-phone technical assistance.

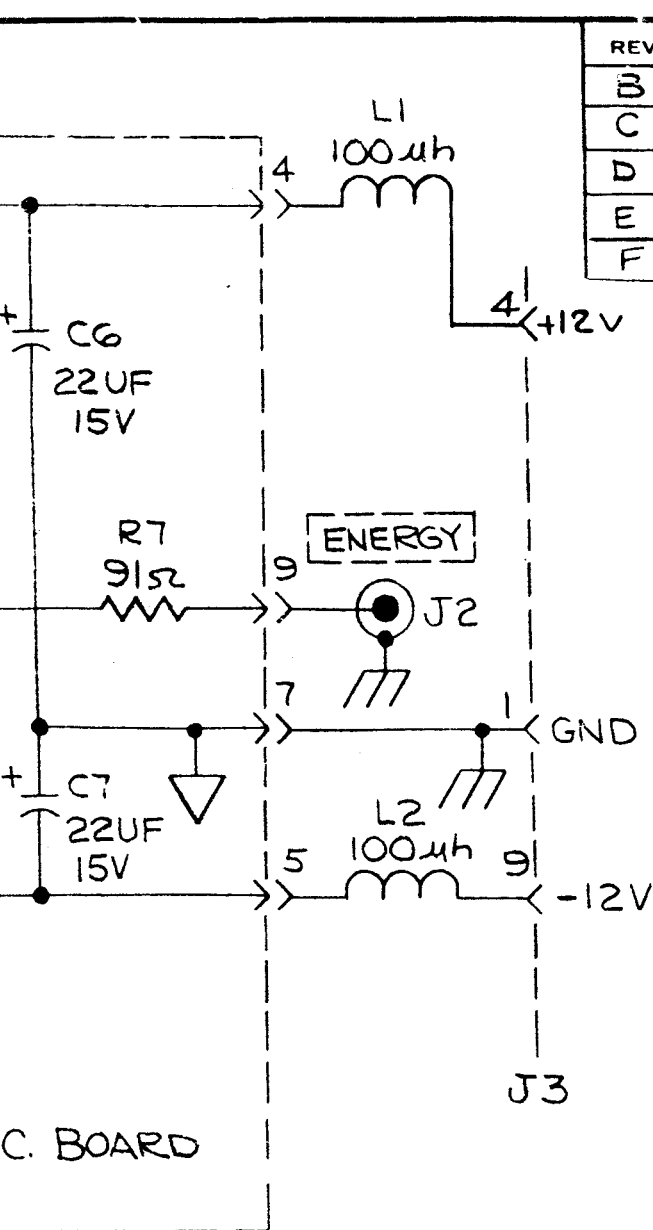
For further information on these service options, please contact any of Canberra's Regional Service Centers.

In addition to our factory-based support services, Canberra's Regional Service Centers are strategically located throughout the world to provide fast and efficient service.





LAST COMPONENT REF. DESIGNATION	
CAPACITORS	C10
DIODES	D1
RESISTORS	R19
CONNECTORS	J4
VARIABLE RESISTORS	RV3
TRANSISTORS	Q2
INDUCTOR	L2

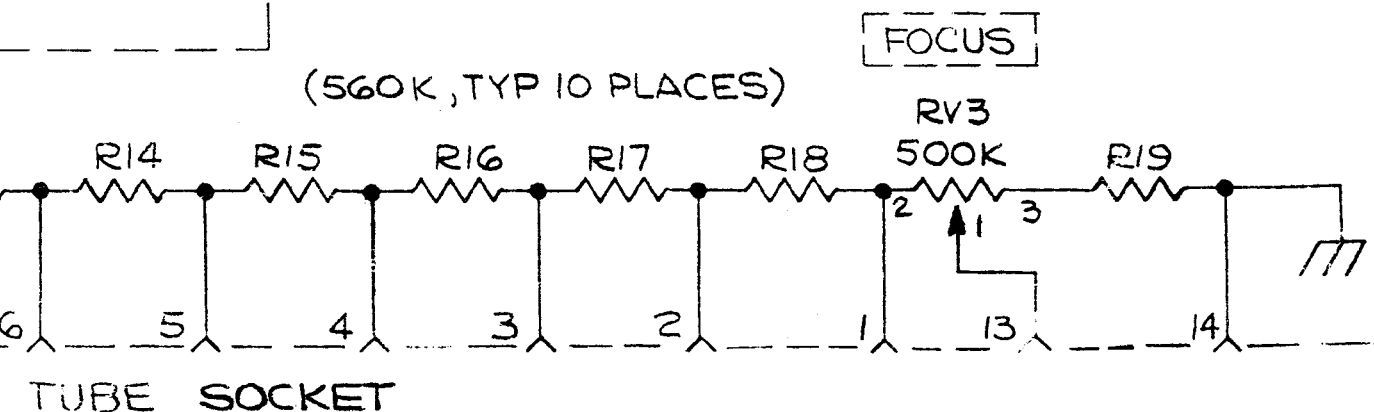


REV	CHANGE	ECN	BY	DATE	APPD
B	REDRAWN & INIT. RELEASE	2049	DRW	12-78	
C	SEE ECN	2060	JH	12-78	
D	REV WIRING ON RV2 SEE ECN	2088	ZP	1-24-78	
E	SEE ECN	2194	AM	4-10-79	
F	AR13002	4418	3AS	2-10-86	
G	REV. C9 & C10 NOW MONO CAP.	5142	HMC	7-21-88	
H	REVISED (AR14080)	5364	RJB	4-19-89	
J	ADD FERRITE BEAD / DELETE MONO CAP.	5397	RA	6-28-89	

#### NOTES:

1. THERE ARE NO FOUR WAY TIES ON THIS SCHEMATIC.
2. UNMARKED RESISTORS ARE  $\frac{1}{4}W$ , 5%.
3. [ ] INDICATES REAR PANEL COMPONENT LOCATION.
4. ■ INDICATES FERRITE BEAD ICN 20300080

C. BOARD



(560K, TYP 10 PLACES)

FOCUS

DRAWN	D. WEST	DATE	12-18-78
CHKD	RW.L.	DATE	12/21/78
APPD MECH			
APPD ELEC	GAH	DATE	12/21/78
NEXT ASSY			
PARTS LIST			
USED ON	A-17405		

SCHEMATIC  
MODEL 2007P

CANBERRA

DRAWING NO	B-17403	REV	0
SHT	1	OF	1

SCALE 1/16

DO NOT TEMPLATE DRAWING